

Introduction to Rheology of complex fluids

Brief Lecture Notes

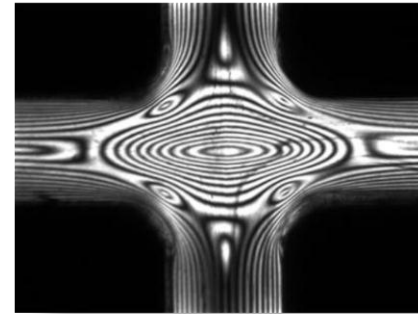
Kinematics and material functions
for extensional flows

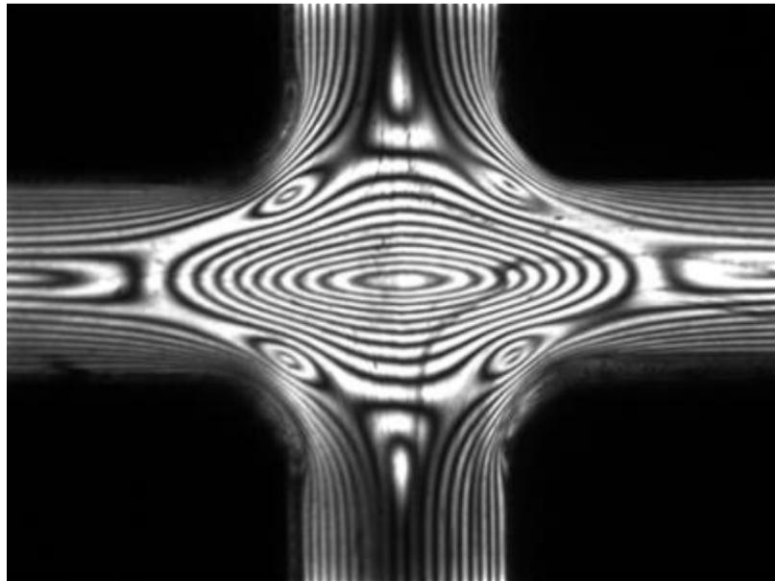


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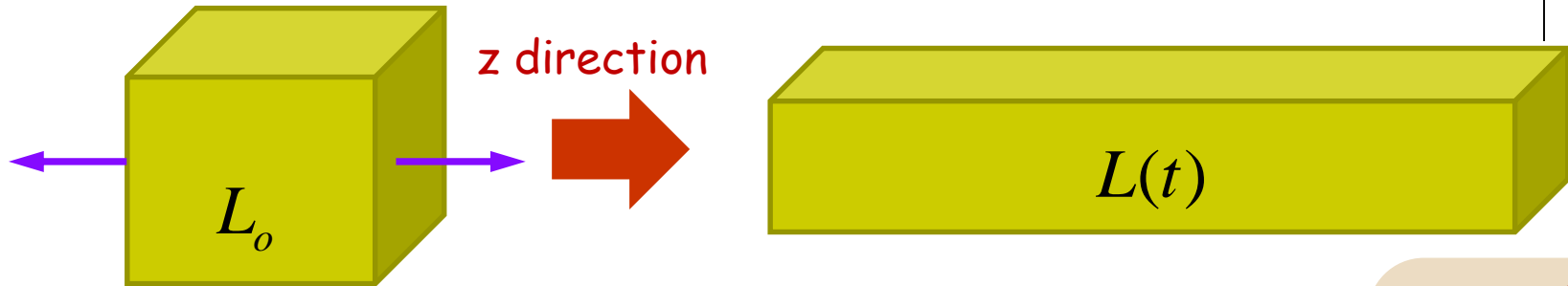
- **Introductory Lecture**
- **Simple Flows**
- **Material functions & Rheological Characterization**
- **Experimental Observations**
- Generalized Newtonian Fluids
- Generalized Linearly viscoelastic Fluids
- Nonlinear Constitutive Models





Kinematics of extensional flow

Deformation in extensional flow



Uniaxial Stretching

$$\varepsilon(t_{ref}, t) = \int_{t_{ref}}^t \dot{\varepsilon}(t') dt'$$

$$= \dot{\varepsilon}_o t$$

$$= \ln \left(\frac{L(t)}{L_o} \right)$$

Hencky Strain

The deformation is proportional to time, when $\dot{\varepsilon}_o = \text{const.}$

The ratio of lengths is an exponential function of time

Nomenclature For Strain

$$\varepsilon \leftrightarrow \gamma$$

$$\varepsilon \leftrightarrow \varepsilon_{zz}$$

Rate of Strain

$$\dot{\varepsilon}_o \leftrightarrow \dot{\gamma}_o$$



Extensional Flow Characteristics

- **Strong**

In comparison to simple shear flow which is a weak flow.

$$L(t) = L_o \exp(\dot{\epsilon}t)$$

Exponential Change

$$z(t) = z(t = 0) + \dot{\gamma}t$$

- **Irrotational**

Recirculations are not formed, while the deformation results from the stretching and the orientation of the macromolecules.

Linear Change

- **Non-viscometric flow**

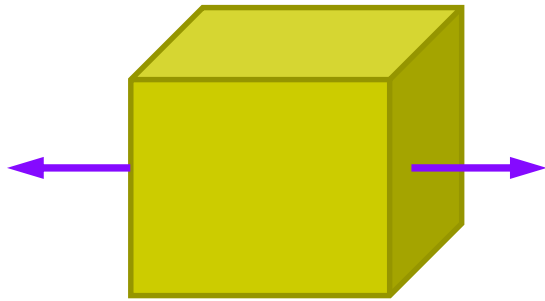
The third invariant of the rate of deformation is non-zero.

- **Three types**

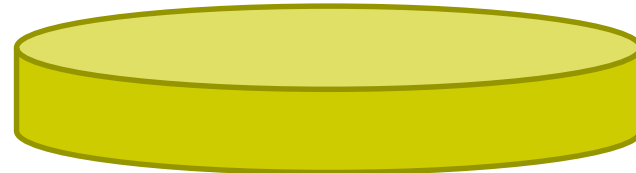
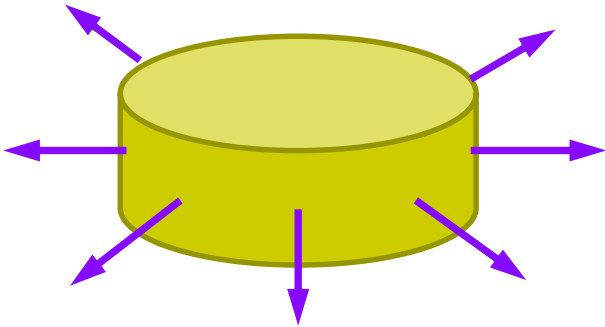
Uniaxial, Biaxial and 2D Elongation



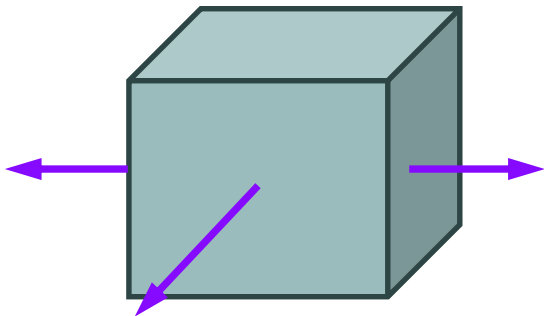
Three Types of Flow



Uniaxial Stretching



Biaxial Stretching



2D Stretching



Three Types of Flow

$$\dot{\epsilon}(t) = \dot{\epsilon}_o = \text{constant}$$

Kinematics

$$v_x(x, y, z) = -\frac{1}{2} \dot{\epsilon}(t)(1+b)x$$

$$v_y(x, y, z) = -\frac{1}{2} \dot{\epsilon}(t)(1-b)y$$

$$v_z(x, y, z) = \dot{\epsilon}(t)z$$

Extension in z direction



Nomenclature

Uniaxial Stretching:

$$b = 0, \quad \dot{\epsilon} > 0$$

Biaxial Stretching:

$$b = 0, \quad \dot{\epsilon} < 0$$

2D Stretching:

$$b = 1, \quad \dot{\epsilon} > 0$$

Three Steady Extensional flows



Rate of Deformation Tensor

$$\underline{\underline{\dot{\gamma}}} = \dot{\epsilon}_o \begin{pmatrix} -\frac{1}{2}(1+b) & 0 & 0 \\ 0 & -\frac{1}{2}(1-b) & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$\underline{\underline{\dot{\gamma}}} = \underline{\underline{\dot{\gamma}}} + (\underline{\underline{\dot{\gamma}}})^T = 2\dot{\epsilon}_o \begin{pmatrix} -\frac{1}{2}(1+b) & 0 & 0 \\ 0 & -\frac{1}{2}(1-b) & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

Nomenclature

$\sigma \longleftrightarrow \tau$

Uniaxial Stretching:

$$b = 0, \quad \dot{\epsilon} > 0$$

Biaxial Stretching:

$$b = 0, \quad \dot{\epsilon} < 0$$

2D Stretching:

$$b = 1, \quad \dot{\epsilon} > 0$$



Three Steady Extensional flows

Material Properties

$$\bar{\eta} \equiv \frac{\tau_{zz} - \tau_{xx}}{\dot{\epsilon}_o}$$

$$\bar{\eta} \Leftrightarrow \bar{\eta}_B \Leftrightarrow \bar{\eta}_{P_1}$$

Uniaxial or Biaxial or 1st
level viscosity

$$\bar{\eta}_{P_2} \equiv \frac{\tau_{yy} - \tau_{xx}}{\dot{\epsilon}_o}$$

2nd level viscosity

Application of Uniaxial Extension In Newtonian Fluids



$$\underline{\underline{\tau}} = \eta \underline{\underline{\dot{\gamma}}}$$

$$\underline{\underline{\dot{\gamma}}} = \underline{\underline{\nabla v}} + (\underline{\underline{\nabla v}})^T = 2\dot{\epsilon} \begin{pmatrix} -1/2 & 0 & 0 \\ 0 & -1/2 & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

$$\tau_{zz} = 2\eta\dot{\epsilon}$$

$$\tau_{yy} = \tau_{xx} = -\eta\dot{\epsilon}$$

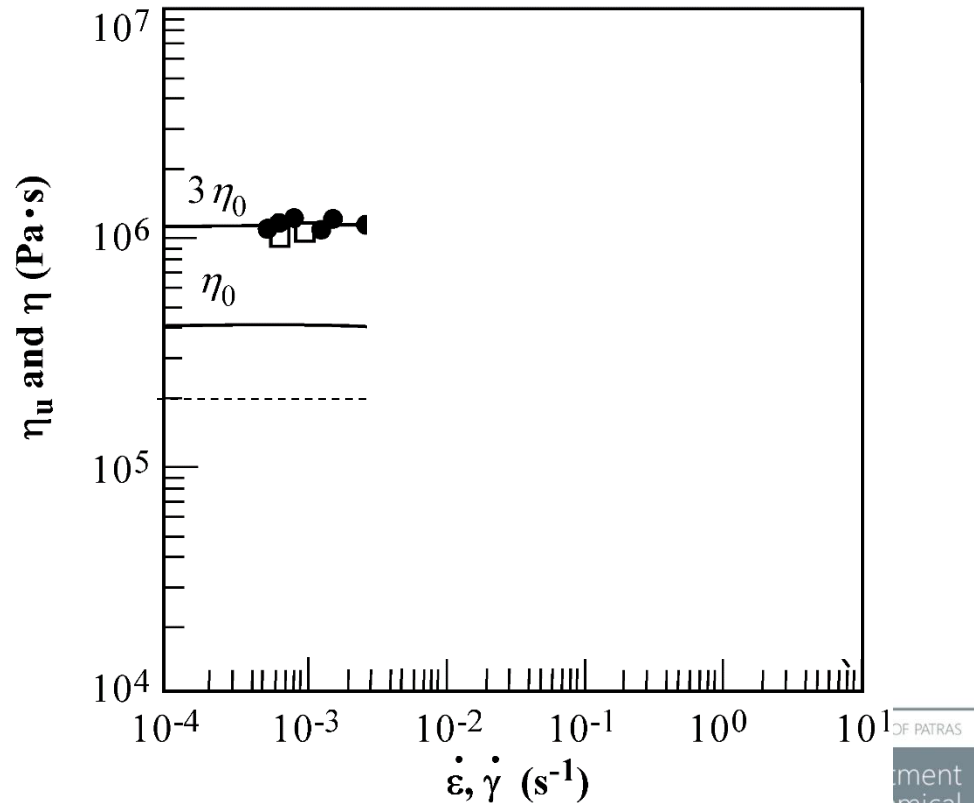
Extensional Viscosity Definition

$$\eta_E(t) = \frac{\tau_{zz} - \tau_{yy}}{\dot{\epsilon}} = 3\eta(t)$$

For low rate of deformation:

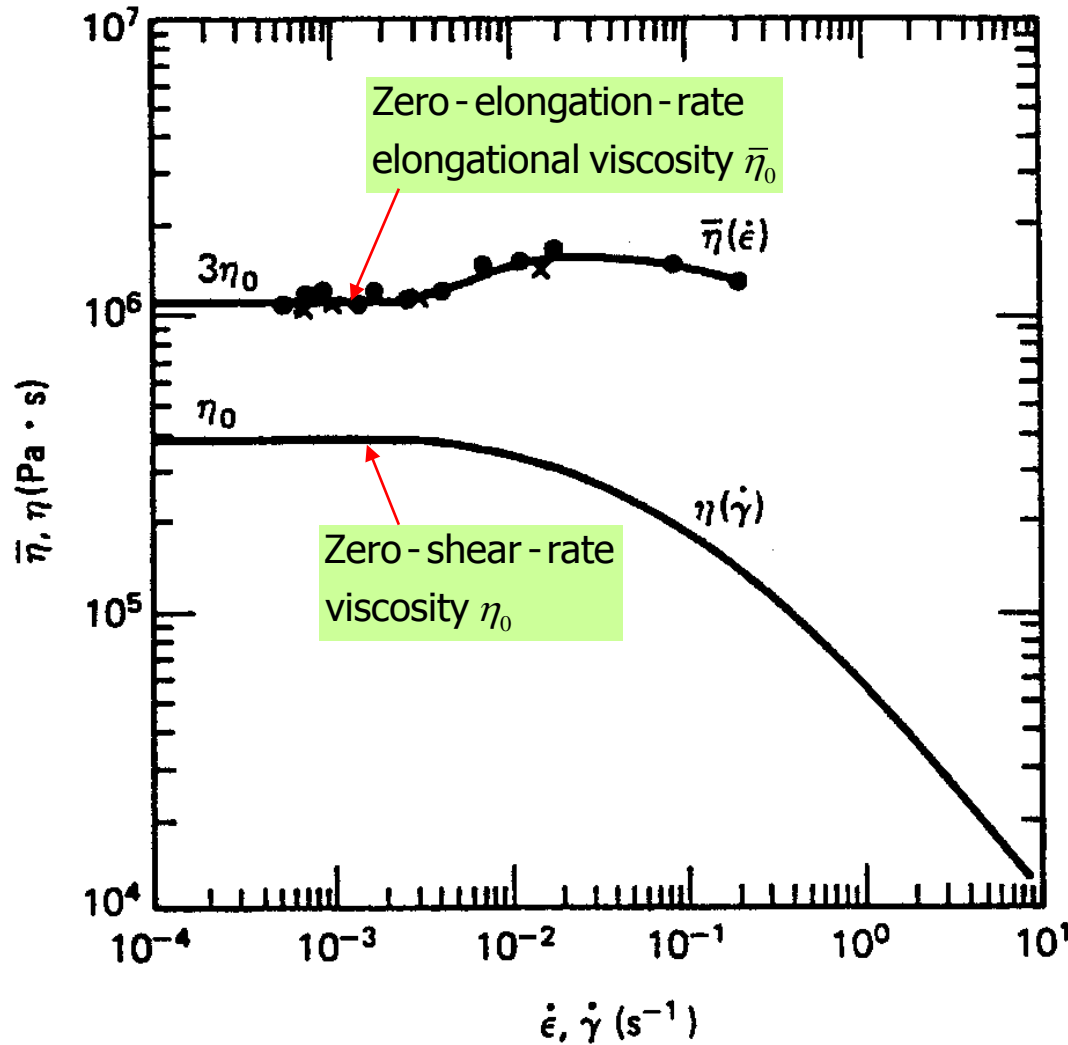
$$\eta_{E,o} = 3\eta_o$$

A lot of materials diverge from this observation



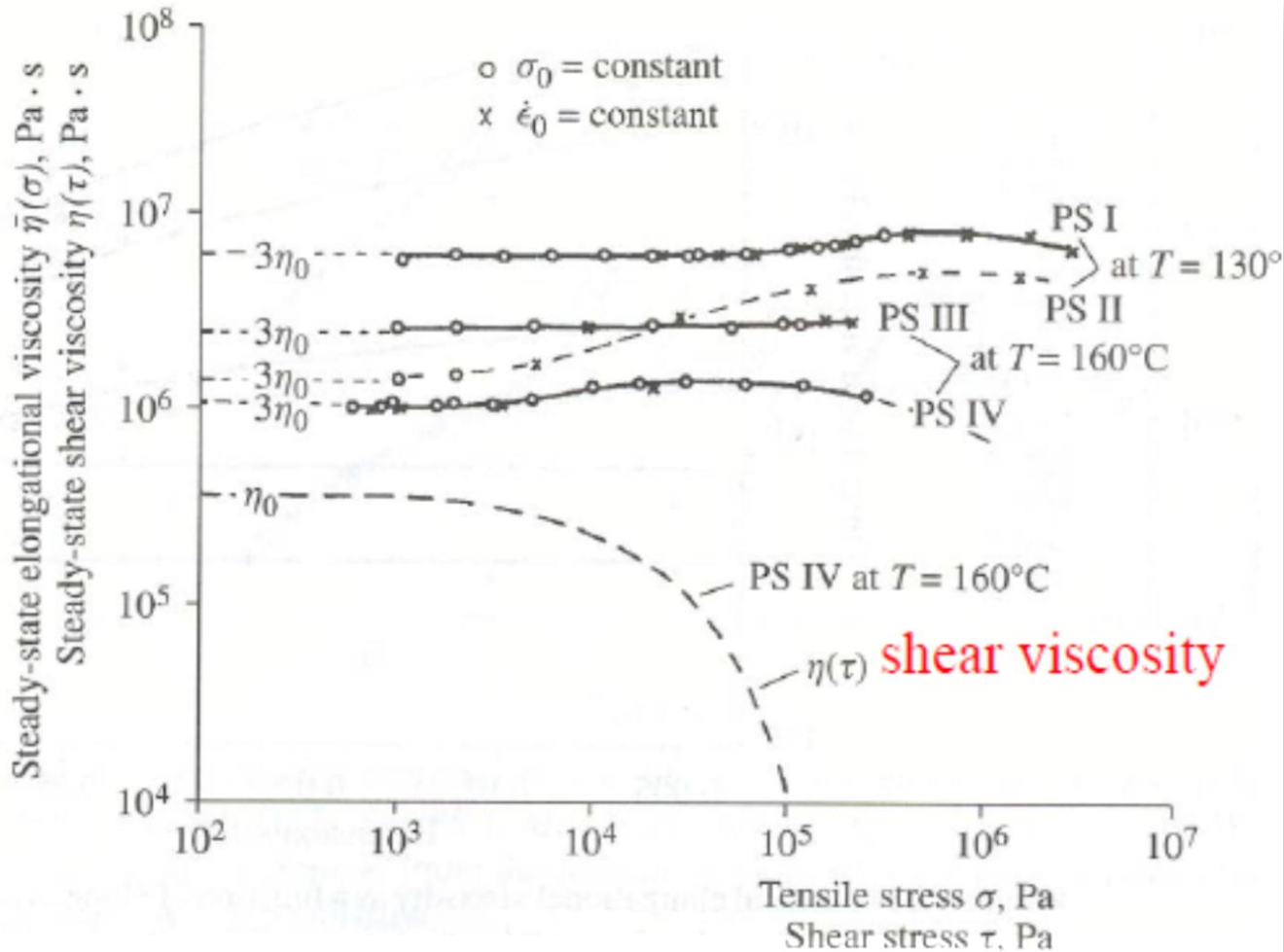


Experimental Observations



Steady elongational and shear viscosity of a PS melt vs. extensional and shear rate of deformation, respectively

Experimental Observations



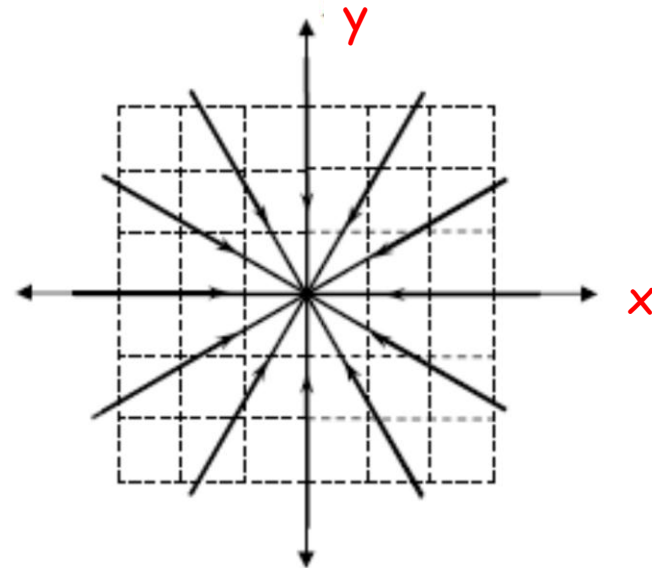
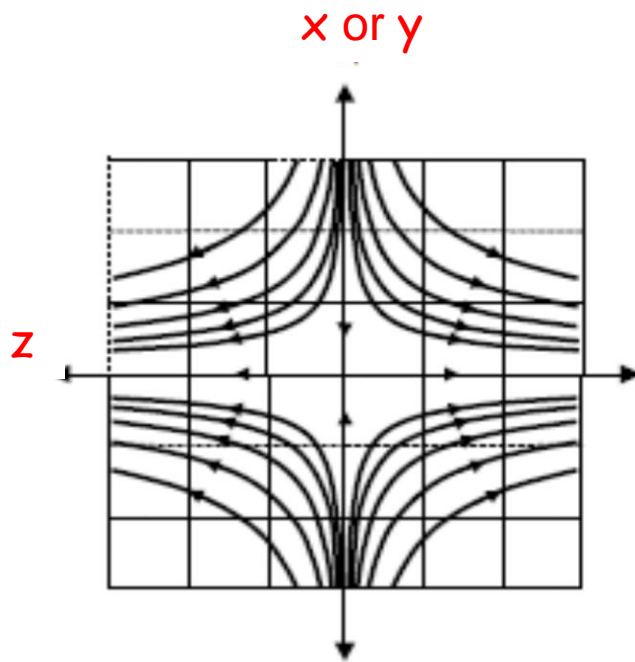
The extensional viscosity first increases and then decreases with increasing $\dot{\epsilon}$.

Trouton Ratio

$$Tr \equiv \frac{\bar{\eta}}{\eta_0}$$



Uniaxial Extensional Flow



Fluid Streaklines



Biaxial Extensional Flow

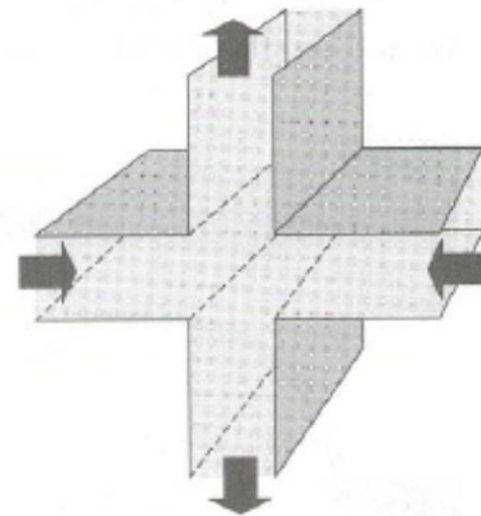
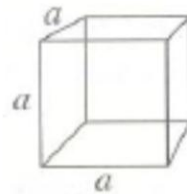
Velocity Field

$$v_x(x, y, z) = -\dot{\epsilon}(t)x$$

$$v_y(x, y, z) = 0$$

$$v_z(x, y, z) = \dot{\epsilon}(t)z$$

Fluid element





Transient Extensional Flows

As in shear flows, in extensional flows a variety of basic and interesting transient patterns have been defined

- **Start-up of Extensional Flows**
- **Cessation of Extensional Flows (almost impossible)**
- **Extensional Creep**
- **Extensional Ramp Deformation**
- **SAOE oscillation of small amplitude**



Extensional Material Properties

Start-up of uniaxial elongation

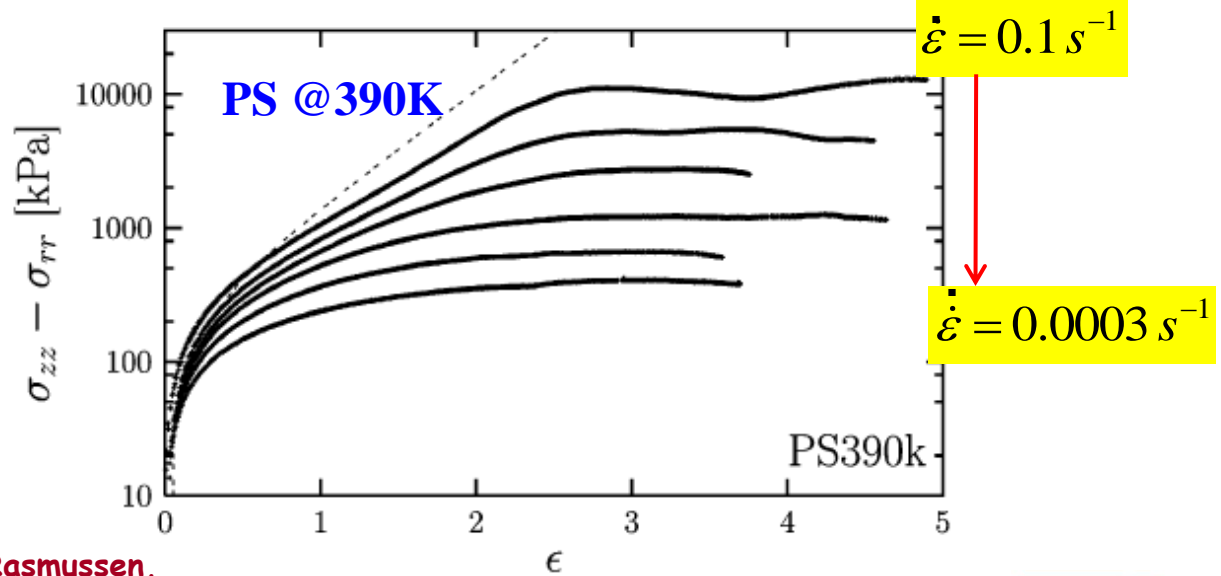
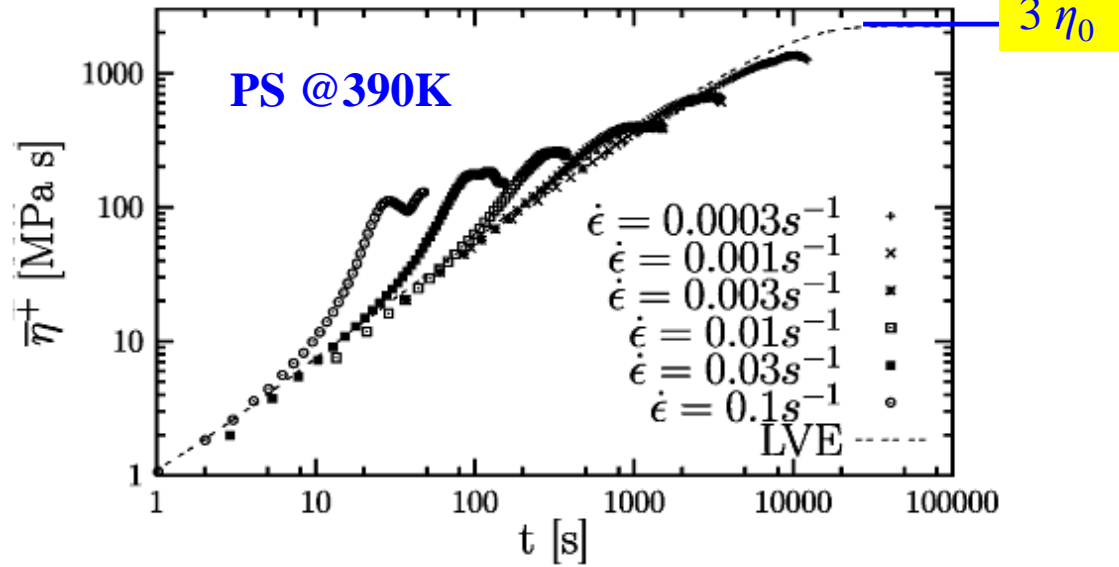
$$\eta_E^+(t, \dot{\epsilon}) = \frac{\tau_E(t, \dot{\epsilon})}{\dot{\epsilon}}$$

$$\tau_E = \tau_{11} - \tau_{22} = \tau_{11} - \tau_{33}$$

In LVE:

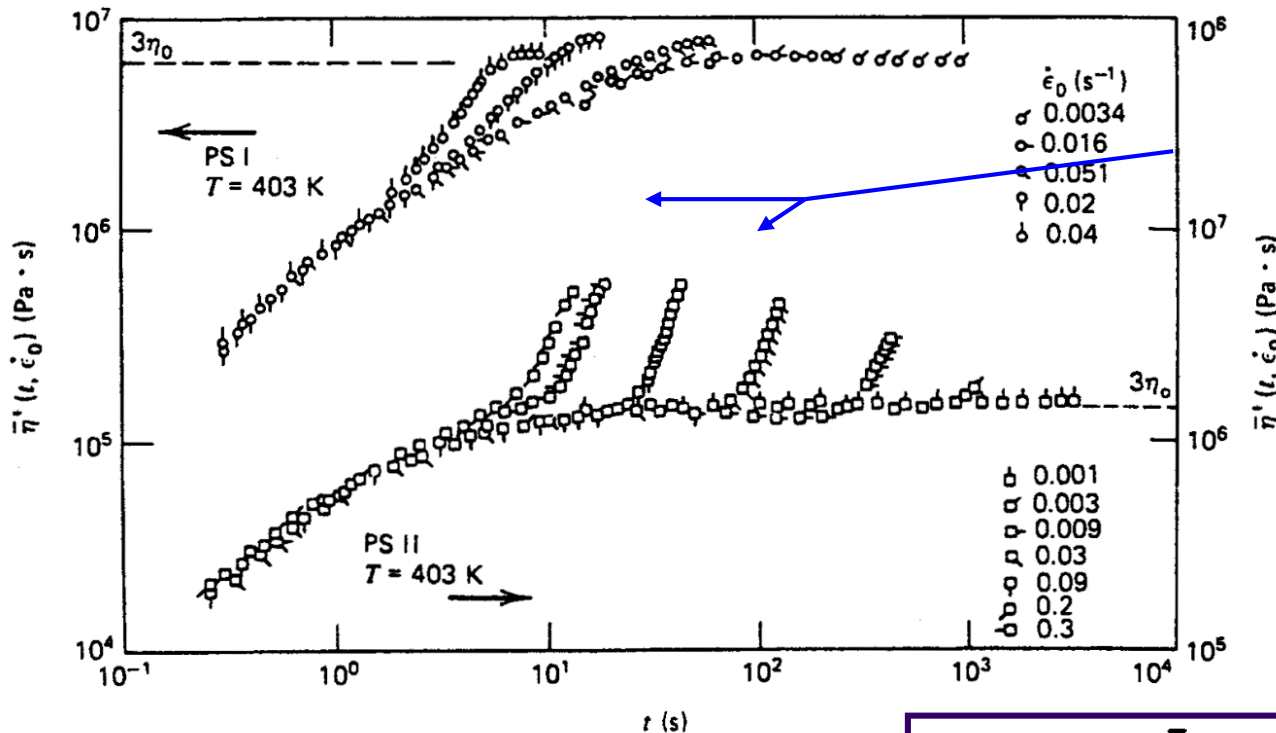
$$\lim_{\dot{\epsilon} \rightarrow 0} \left\{ \eta_E^+(t, \dot{\epsilon}) \right\} = \eta_{E,o}^+(t) = 3\eta_o^+(t)$$

Startup of extensional flow



A. Bach, K. Almdal, H. K. Rasmussen,
O. Hassager, *Macromolecules* 36,
5174-5179 (2003)

Start-up of Extensional Flow



Extensional increase of the viscosity in constant value of Hencky strain:

$$\epsilon(0, t) = \dot{\epsilon}_0 t$$

Molecular Weight of the samples:

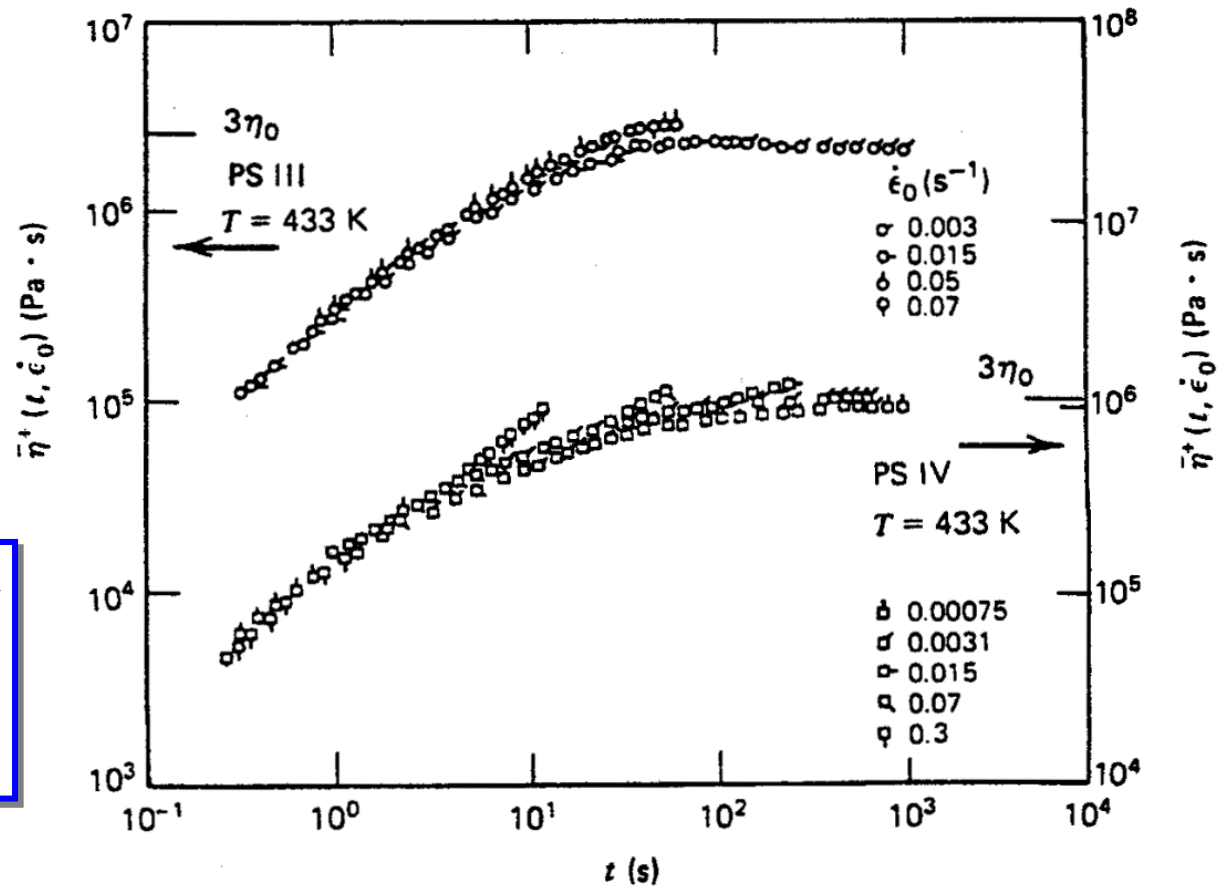
	\bar{M}_w	\bar{M}_w/\bar{M}_n
PS I	7.4×10^4	1.2
PS II	3.9×10^4	1.1
PS III	2.53×10^5	1.9
PS IV	2.19×10^5	2.3

Monodisperse

Start-up of Extensional Flow



	\bar{M}_w	\bar{M}_w/\bar{M}_n
PS I	7.4×10^4	1.2
PS II	3.9×10^4	1.1
PS III	2.53×10^5	1.9
PS IV	2.19×10^5	2.3





Extensional Material Properties

Start-up of biaxial elongation

$$\eta_B^+(t, \dot{\epsilon}_B) = \frac{\tau_B(t, \dot{\epsilon}_B)}{\dot{\epsilon}} \quad \tau_B = \tau_{11} - \tau_{22} = \tau_{11} - \tau_{33}$$

In LVE:

$$\lim_{\dot{\epsilon}_B \rightarrow 0} \left\{ \eta_B^+(t, \dot{\epsilon}_B) \right\} = \eta_{B,o}^+(t) = 6\eta_o^+(t)$$



Extensional Material Properties

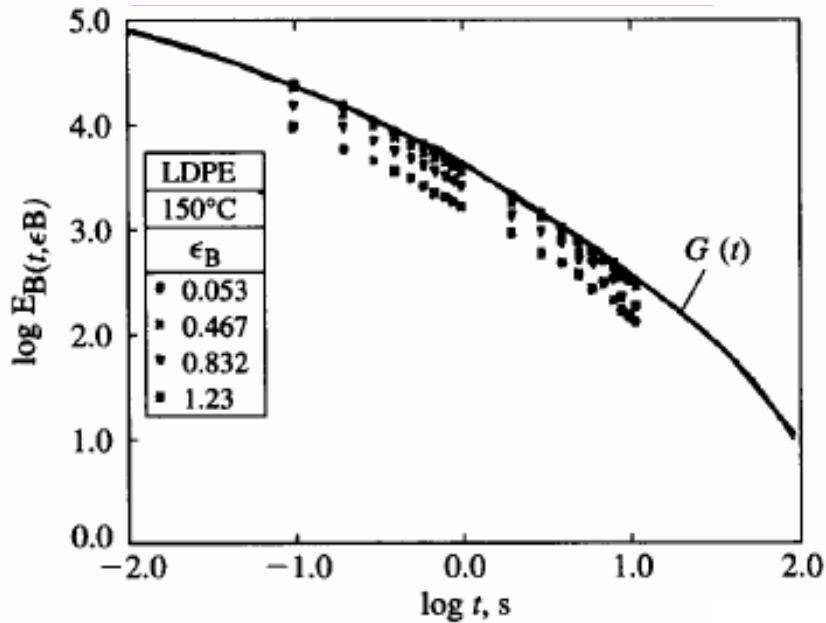
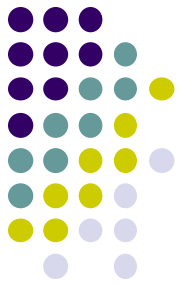
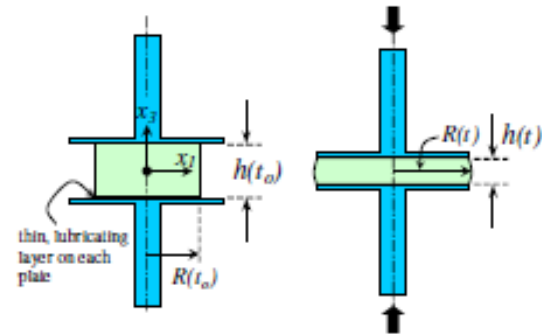
Start-up of 2D elongation

$$\eta_{p_1}^+(t, \dot{\epsilon}_B) = \frac{\tau_{11} - \tau_{33}}{\dot{\epsilon}} \quad \eta_{p_2}^+(t, \dot{\epsilon}_B) = \frac{\tau_{22} - \tau_{33}}{\dot{\epsilon}}$$

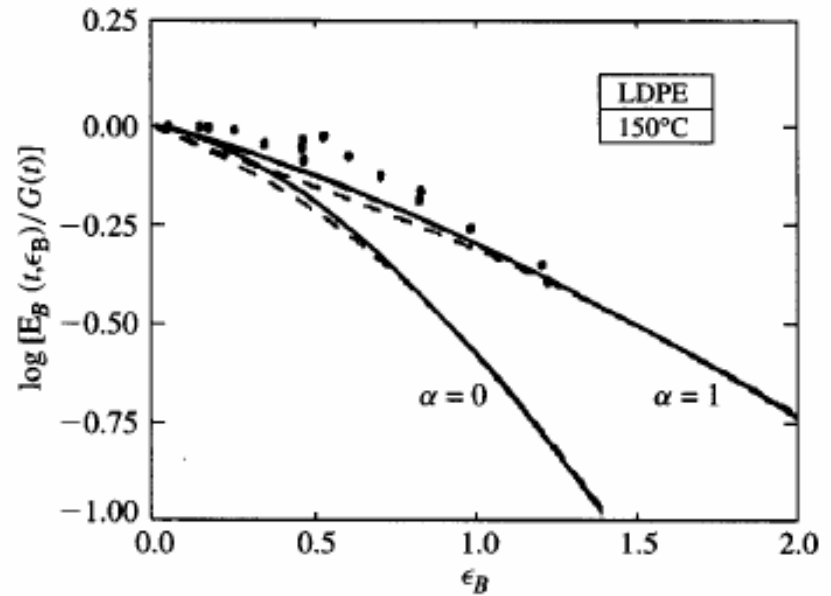
In LVE:

$$\eta_{p_1,o}^+(t, \dot{\epsilon}_B) = 4\eta_o^+(t_B) \quad \eta_{p_2,o}^+(t, \dot{\epsilon}_B) = 4\eta_o^+(t_B)$$

Extensional Flow due to Step Deformation



Deformation function for biaxial flow



Damping function for biaxial flow



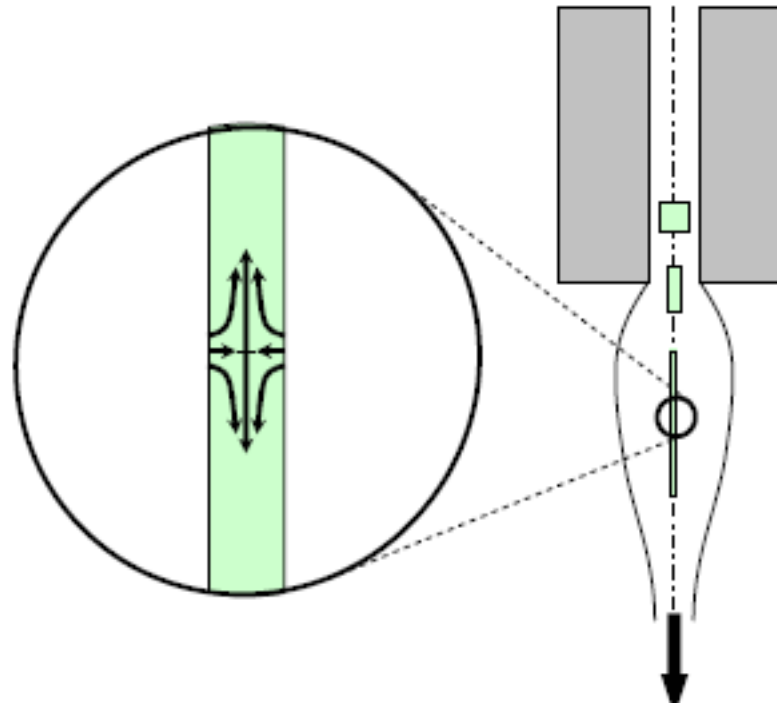
Transient Rheological Parameters

Parameter	Shear	Elongation	Units
Strain	$\gamma = \gamma_0 \sin(\omega t)$	$\epsilon = \epsilon_0 \sin(\omega t)$	---
Stress	$s = s_0 \sin(\omega t + \delta)$	$t = t_0 \sin(\omega t + \delta)$	Pa
Storage Modulus (Elasticity)	$G' = (s_0/\gamma_0) \cos \delta$	$E' = (t_0/\epsilon_0) \cos \delta$	Pa
Loss Modulus (Viscous Nature)	$G'' = (s_0/\gamma_0) \sin \delta$	$E'' = (t_0/\epsilon_0) \sin \delta$	Pa
Tan δ	G''/G'	E''/E'	---
Complex Modulus	$G^* = (G'^2 + G''^2)^{0.5}$	$E^* = (E'^2 + E''^2)^{0.5}$	Pa
Complex Viscosity	$\eta^* = G^*/\omega$	$\eta_E^* = E^*/\omega$	Pa-sec



Why Extensional flow is a Rheological Flow?

- Simple Flow Field
- Represents many similar, but more complex flows
- Simple expression of the stress tensor



Comments on the Extensional Flows



Steady Deformation

- Difficulties in reproducing the experiments
- Difficulties even in the steady extensional flows
- Important for many practical processes

Non Steady Deformation

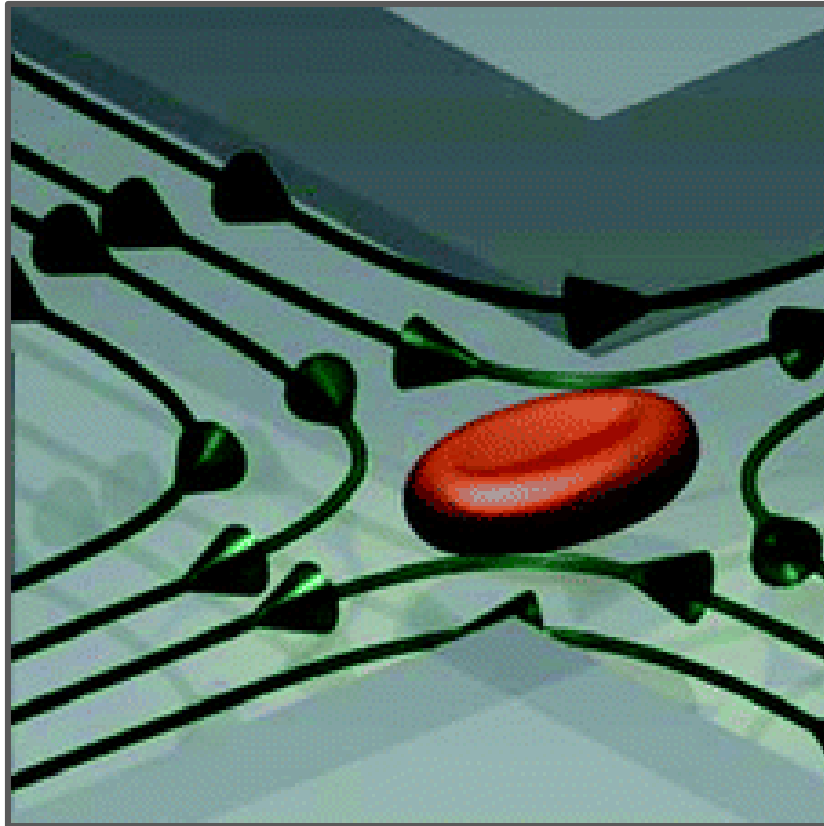
- Difficulties in reproducing the experiments
- Open Question: What is the quantitative increase of stresses with the deformation (strain hardening)



Why have we chosen these flows?

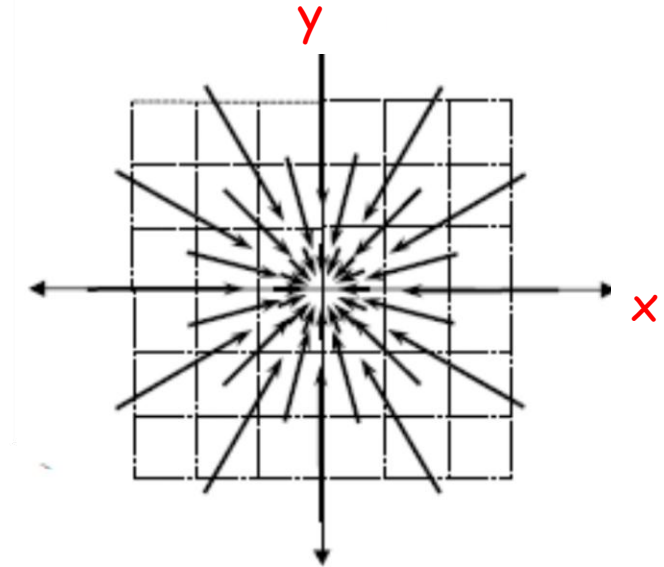
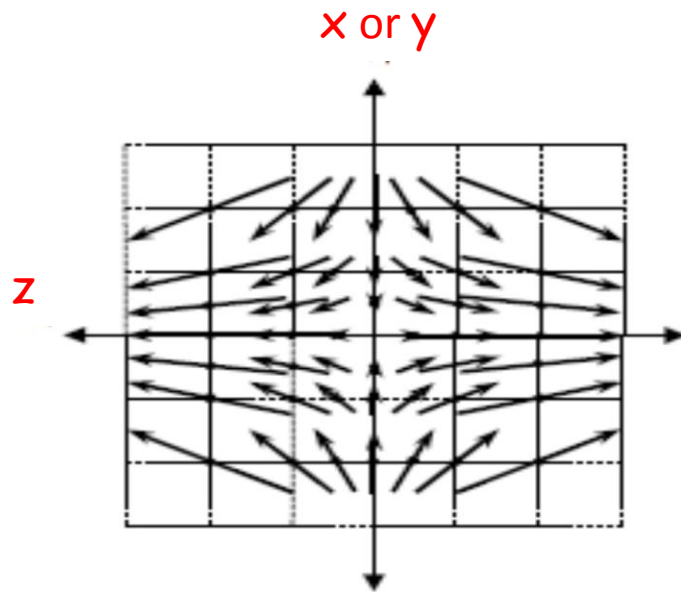
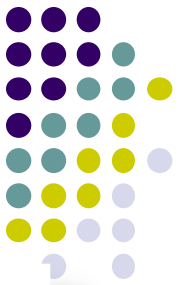
Because they are **symmetric**.

Symmetry facilitates reaching conclusions for the stress tensor that produces these well-described flow fields **for each different fluid**.



End of
lecture

Uniaxial Extensional Flow

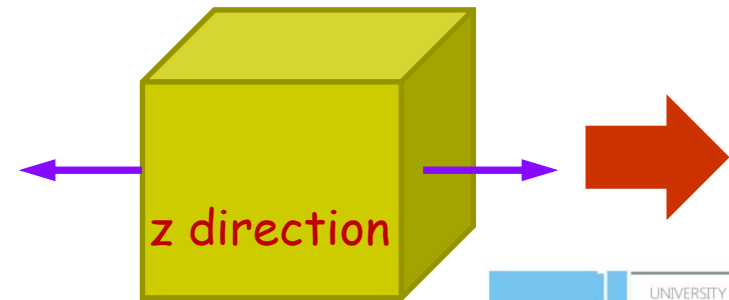


Velocity Field

$$v_x(x, y, z) = -\frac{\dot{\epsilon}(t)}{2} x$$

$$v_y(x, y, z) = -\frac{\dot{\epsilon}(t)}{2} y$$

$$v_z(x, y, z) = \dot{\epsilon}(t) z$$



Uniaxial Extension

Start-up of Extensional Flow

Extensional Increase of the viscosity

Fitting with Pom-Pom model

